

Article

The Monitoring of H₂S and SO₂ Noxious Gases from Industrial Environment with Sensors Based on Flame-spray-made SnO₂ Nanoparticles

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Abstract. The noxious gas sensors were developed successfully using flame-spray-made SnO₂ nanoparticles as the sensing materials. The functionalized nanoparticle properties were further analyzed by XRD, BET and TEM analyses. The SnO₂ nanoparticles (SSA_{BET} : 141.6 m²/g) were investigated revealing non-agglomerated spherical, hexagonal, rectangle (3–10 nm), and rod-like (3–5 nm in width and 5–20 nm in length) morphologies. The sensing films were prepared by spin coating onto the Al₂O₃ substrates interdigitated with Au electrodes. The sensing films were significantly developed in order to detect with H₂S (0.5–10 ppm) and SO₂ (20–500 ppm) at the operating temperature ranging from 200–350°C. After sensing test, the cross-section of sensing film was analyzed by SEM analyses. It was found that SnO₂ sensing film showed higher sensitivity to H₂S gas with very fast response at lower concentrations (3s, to 10 ppm). The cross sensitivities of the sensor towards different concentrations of H₂S, CO, H₂, and C₂H₂ were measured at 300°C. The sensor evidently shows much less response to CO, H₂, and C₂H₂ than to H₂S indicating higher selectivity for H₂S of the SnO₂ sensor at the lower concentration (10 ppm). Therefore, the SnO₂ sensor was the most suitable candidate for the efficient detection of H₂S noxious gas.

Keywords: H₂S, SO₂, noxious gas, environmental sensors, SnO₂, flame spray pyrolysis.

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1. Introduction

Hydrogen sulfide (H₂S) is a toxic gas produced from the coal, oil, and natural gas industries [1–7]. The high toxicity of H₂S, which has significant negative impacts on health and the environment, has attracted attention to monitor and control this gas. With a maximum allowed limit in the atmosphere of 10 ppm H₂S [6], developing reliable sensors with high sensitivity and also selectivity towards other gases is a real challenge. Sulfur dioxide (SO₂) gas is one of the most toxic and common air pollutants [4, 8, 9]. Due to growing concern on environmental issues, much attention has been focused on the monitoring of air pollutants. SO₂ is one of the major gases that cause a serious air pollution problem. The most important application falls in the category where human beings cannot afford to risk smelling noxious gases. Also, an exposure to SO₂ can cause irritation to eyes, skin and respiratory system. These are the reason for increasing requirements to monitor the gas pollutions in urban agglomerates or in the work ambient atmosphere [8, 9]. The long-term exposure limit and the short-term exposure limit of sulfur dioxide gas are 2–5 ppm, respectively, although the acceptable limit of SO₂ in ambient air is much less. Nevertheless, the monitoring of SO₂ leakage at the source may be helpful to contain not only the accidental exposure at the source but also environmental pollution in general [8, 9]. Therefore, rapid detections of poisonous and hazardous gases including H₂S and SO₂ in technological wastes are challenging.

Recently, metal oxide semiconductors (MOS) [10–17] have been extensively investigated for this purpose due to their simplicity, small dimensions and attractive price. Several types of metal oxide semiconductors have been used as sensing material for different type of gases. SnO₂ is one of the most promising materials for sensor and has attractively established the attention of many users and scientists' interest in gas sensing under atmospheric conditions. It is a wide band gap and the best-understood prototype of oxide-based gas sensors for the detection of various noxious gases especially H₂S and SO₂ [1–9]. In the present study, Flame Spray Pyrolysis (FSP) is presented as a very promising technique for sensor material fabrication since it enables primary particle and crystal size control [18, 19], which is important to improve the sensitivity, as well as controlling in situ deposition of noble metal clusters [19]. It has been shown that due to the morphology of the FSP-made particles, the mass transfer rates in catalysis are higher compared to microporous material because of the large external surface area of flame-made materials [19, 20]. Moreover, the importance of the size control, the required large and easily accessible surface area (large pore size, no micropores), the efficiency of noble metal doping, and competitive production rates put high demands on the method of nanoparticles production for sensor materials. Therefore, it is interesting to apply FSP for production of SnO₂ nanoparticles to be used in environmental gas sensors. In this work, the applicability of FSP in synthesis of SnO₂ nanoparticles for noxious gas sensing from industrial environment is reported. The aim is to demonstrate that the FSP process in general can be successfully applied for sensor material production and to specifically evaluate the noxious i.e. H₂S and SO₂ performance of environmental gas sensors.

2. Experimental

2.1. Flame Synthesis

Figure 1 shows the set up for FSP process used to produce the flame-spray-made SnO₂ nanopowders. Precursor solutions (0.50 M) were prepared by dissolving appropriate amounts of tin (II) 2-ethylhexanoate (Aldrich, 95%) used as Sn in xylene (Carlo Erba, 98.5%). The precursor mixture was fed into a nozzle at a constant feed rate of 5 ml/min using a syringe pump. At the end of the nozzle the precursor solution was dispersed by 4.30 l/min oxygen forming a spray with a pressure drop at the capillary tip kept constant at 1.5 bars by adjusting the orifice gap area. A sheath gas flow of 3.92 l/min of O₂ was supplied concentrically around the nozzle to stabilize and control the spray flame. The spray was ignited by supporting flamelets fed with oxygen (2.46 l/min) and methane (1.19 l/min), which were positioned in a ring around the nozzle outlet. The observed flame height was approximately 10 cm and appearance was light orange. The combustion enthalpies were directly dependent on the particular solvent, starting materials. After evaporation and combustion of precursor droplets, particles were formed by nucleation, condensation, coagulation, and coalescence. Finally, the nanopowders were collected on a glass microfibre filters (Whatmann GF/A, 25.7 cm in diameter) with the aid of a vacuum pump (Busch, Seco SV 1040C).

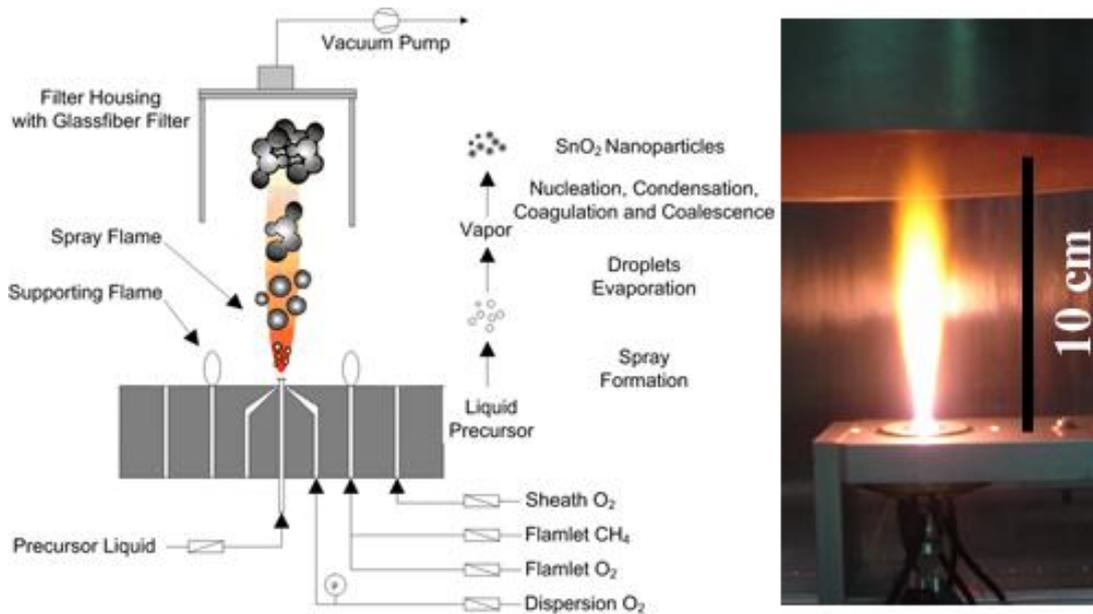


Fig. 1. Schematic diagram of FSP process and flame appearance.

2.2. Nanopowder Characterizations

The nanopowders phase was analyzed by X-ray diffraction (XRD) [Phillips X- μ pert] using CuK α radiation (20 kV, 20 mA) with a scanning speed of 5°/min. The Brunauer-Emmett-Teller (BET) specific surface area (SSA_{BET}), was measured by nitrogen adsorption at 78 K [Autosorb 1 MP, Quantachrome] after degassing at 120°C for 2h prior to analysis in nitrogen. Assuming uniform spherical particles within an aggregate, the average equivalent diameter of the primary particles was calculated from $d_{BET} = 6/SSA_{BET} \times \rho_{sample}$, where SSA_{BET} was the specific surface area (m²/g) and ρ_{sample} was the average density of SnO₂ ($\rho_{SnO_2} = 6.85$ g/cm³ [10]). The accurate morphologies of the SnO₂ nanoparticles were determined by transmission electron microscopy (TEM) [JSM-2010, JEOL]. After sensing test, the cross-sectional structures of sensor were observed by scanning electron microscopy (SEM) [JSM-6335F, JEOL] analyses.

2.3. Sensor Preparation

An appropriate quantity of 0.28 mL homogeneous mixed solution was prepared by stirring and heating at 80°C for 12h with ethyl cellulose (Fluka, 30–70 mPa.s) as the temporary binder and terpineol (Aldrich, 90%) as a solvent. The liquid mixture was combined with 60 mg samples of the flame-made SnO₂ nanopowders and mixed for 30 min to form a paste prior to spin-coating. The resulting paste was firstly spin-coated at 700 rpm for 10 s, and then subsequently at 3,000 rpm for 30 s on the Al₂O₃ substrates (0.4 × 0.5 × 0.1 cm) interdigitated with Au electrodes to deposit sensing films. The resulting substrates were annealed in an oven at 150°C for 1h with an annealing rate of 1°C/min and then subsequently annealed at 400°C for 1h with an annealing rate of 1°C/min for binder removal prior to the sensing test.

2.4. Noxious Gases Sensing Measurements

The gas-sensing characteristics of SnO₂ sensing films were characterized over a high concentration range of SO₂ (20–500 ppm). In contrast, it was tested specifically within a low concentration range of H₂S (0.5–10 ppm). The standard flow through technique was used to test the gas-sensing properties of SnO₂ films. A constant flux of synthetic air of 2 l/min as gas carrier was flowed to mix with desired concentration of pollutants dispersed in synthetic air. All measurements were conducted in a temperature-stabilized sealed chamber at 20°C under controlled humidity. The gas flow rates were precisely manipulated using a computer controlled multi-channel mass flow controller. An external NiCr heater was heated by a regulated DC power supply to different operating temperatures ranging from 200–350°C. The resistances of various sensors were continuously monitored with a computer-controlled system by voltage-amperometric

technique with 10 V DC bias and current measurement through a picoammeter. The sensor was exposed to a gas sample for ~ 5 minutes for each gas concentration testing and then the air flux was restored for 15 minutes. The sensitivity (S) is defined as the resistance ratio R_a/R_g , where R_a is the resistance in dry air, and R_g is the resistance in the test gas. After sensors fabrication, they had been tested with varied the operating temperatures. Finally, the sensing film morphology were observed using SEM analysis.

3. Results and Discussion

3.1. Particle Properties

Figure 2 shows the XRD patterns of flame-spray-made SnO_2 nanopowders. It can be seen that the nanopowders were highly crystalline and all peaks can be confirmed to be the cassiterite-tetragonal phase of SnO_2 from their excellent matching to the JCPDS file NO. 77-447 [symmetrical group: $P_{42/mnm}$] with lattice constants of $a=b=0.4735$ nm and $c=0.3185$ nm. Figure 3 illustrates the TEM bright-field image of flame-spray-made pure SnO_2 nanoparticles. The corresponding electron diffraction pattern is shown in the inset. From the TEM bright-field image, SnO_2 primary nanoparticles are polyhedral, non-agglomerated and well dispersed. In addition, flame-spray-made SnO_2 nanoparticles indicate polyhedral aggregates of primary particles. The morphologies of flame made (5/5) SnO_2 and 0.2–3 wt% Ru/ SnO_2 nanoparticles contain mainly spherical particles with diameters ranging from 3–10 nm, and occasionally rectangular, hexagonal (3–10 nm) and rod-like (3–5 nm in width, and 5–20 nm in length) particles. From the measured SSA_{BET} for SnO_2 nanoparticles of 141.6 m^2/g , the average BET-equivalent particle diameter is determined to be 6.2 nm. The particle diameters from BET and TEM analysis are in good agreement ($d_{\text{BET}} = 6.2$ nm, $d_{\text{TEM}} = 3\text{--}10$ nm). The small primary-particle size and correspondingly large specific surface area of flame-spray-made SnO_2 nanoparticles are highly preferred properties for gas-sensing.

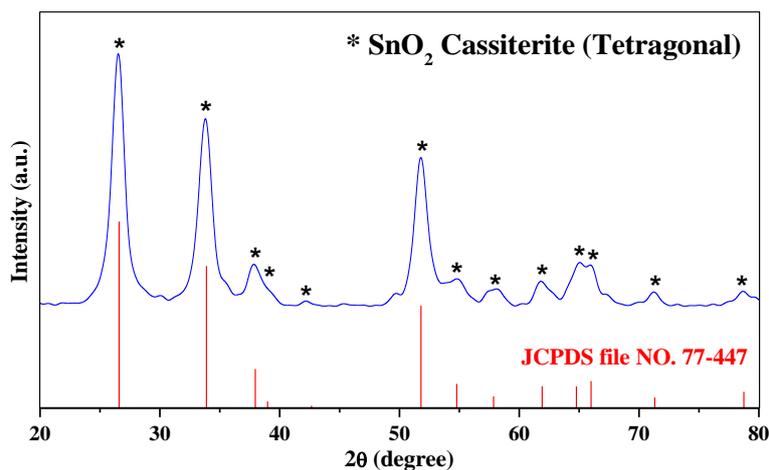


Fig. 2. XRD patterns of flame-spray-made unloaded SnO_2 nanoparticles.

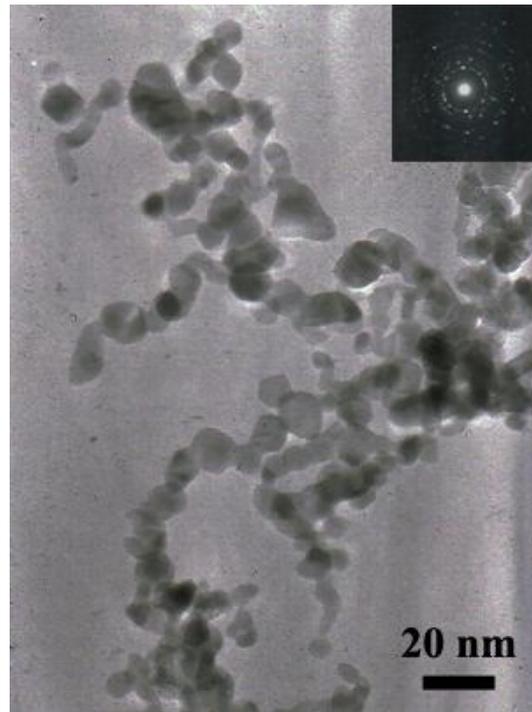
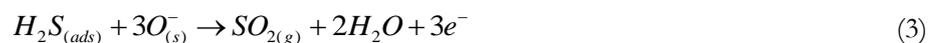
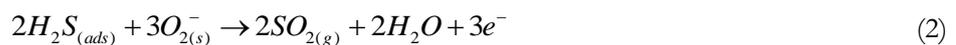


Fig. 3. TEM bright-field image of flame-spray-made unloaded SnO₂ nanoparticles. Non-agglomerated particles can be observed. The corresponding electron diffraction pattern was shown in the inset.

3.2. Noxious Gases (SO₂ and H₂S) Sensing Properties

Figure 4 shows the variation of the sensitivity to H₂S concentration ranging from 0.5–10 ppm with different operating temperatures. It is observed that the sensitivity towards H₂S increases with temperature and attains a maximum value at 300°C, followed by declining with further increase in the operating temperature. It is observed that the SnO₂ sensing films responded to 10 ppm exhibits the highest sensitivity (8.4) to H₂S at 300°C. SnO₂ is an n-type semiconductor in which the adsorbed oxygen reacts with the combustible gas releasing electrons into the conduction band by which the conductivity increases. When the sensors are exposed to air atmosphere, oxygen will be physically and chemically adsorbed on the surface of SnO₂ sensing film. The adsorbed oxygen molecules act as electron acceptors and then form O^{2-} , O_2^- , O^- , generating depleted layers resulting in the release of the large number of free electrons as followed by Eqs. (1–3). The increase of the width and height of the potential barrier at the contacts among nanocrystals and consequently lead to resistance increase of the sensors. Moreover, H₂S is also chemisorbed on the surface and the metal oxide is chemically transformed into sulfides as shown in Eq. (4).



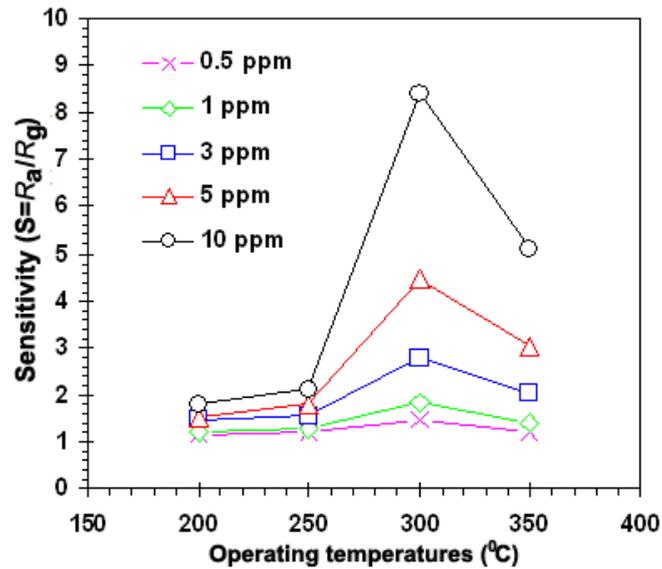


Fig. 4. Variation of the sensitivity to 0.5–10 ppm of H₂S with different the operating temperatures ranging from 200–350°C.

The interaction of the resistive sensors with a target gas produces a change in the electrical conductance of the sensors recorded by a variation in the electrical resistance. Figure 5 shows the change in resistance of SnO₂ sensors under exposure to H₂S pulses with varying concentrations from 0.5 to 10 ppm at operating temperatures ranging from 200–350°C during backward cycle. The resistance reduction is clearly seen at all gas concentrations indicating that the SnO₂ sensor has typical n-type semiconductor behaviors. It can be noticed that the operating temperature at 300°C shows the best response with evident decreasing the resistance than the other operating temperatures. Thus, this suitable operating temperature can greatly improve H₂S response of SnO₂ sensors. In addition, SnO₂ sensor had fast response with rather stable in recovery baseline even at low operating temperature of 300°C.

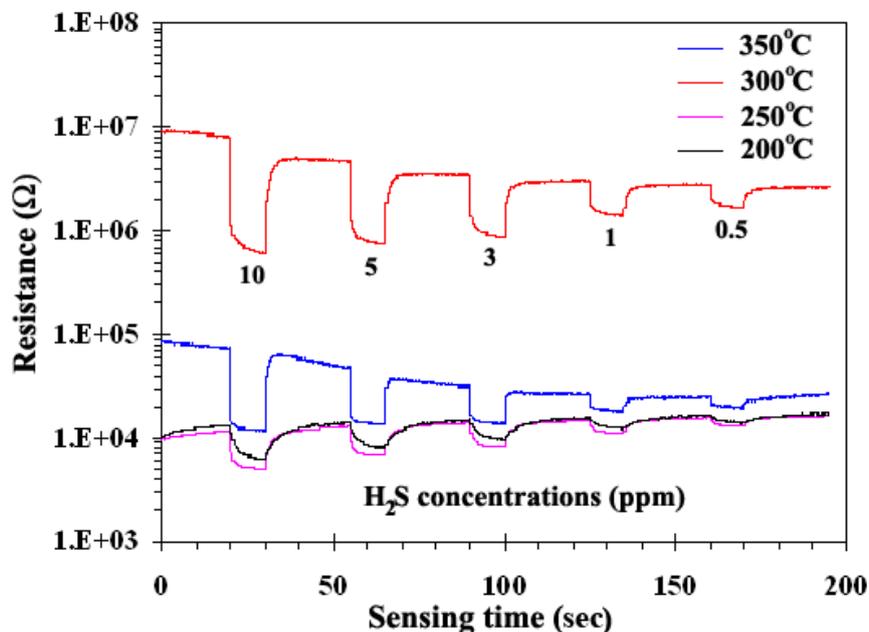


Fig. 5. Change in resistance of SnO₂ sensor upon exposure to H₂S at operating temperatures ranging from 200–350°C.

Figures 6(a) and 6(b) show the plot of response (S) and response times (T_{res}) for the SnO₂ sensor versus concentrations of noxious H₂S (0.5–10 ppm, Fig. 6(a)) and SO₂ (20–500 ppm, Fig. 6(b)) gases at operating temperatures ranging from 200–350°C. In Fig. 6 (a), it was clear that the responses (left) increased and the response times (right) drastically decreased with increasing H₂S concentrations. For both H₂S and SO₂ (Figs. 6 (a) and 6 (b)), it can be seen that sensor had the best sensing performances at 300°C than the other operating temperatures with the highest response and the shortest response times. The better H₂S sensing performance in terms of the response ($S=8.4$) and response time (3 s) are obtained at the highest concentration (10 ppm) at 300°C, while the response ($S=6.9$) and response time (12 s) to higher concentration of 500 ppm were considerably lower (Fig. 6 (b)) through performed higher concentration. The SnO₂ sensor shows very fast response to H₂S whereas the responses to SO₂ are somewhat sluggish. While the sensor reveals quite low SO₂ response at 500 ppm, H₂S sensing yields much higher response at lower concentration, enabling more accurate detection of the small leakage in an atmosphere form the industrial environment. The superior sensitivity toward H₂S may be explained from the reaction kinetic of H₂S and SO₂ according to the reaction paths (1) and (5):



It can be seen that H₂S molecule can produce three times of the number of free electrons per reaction compared to that of SO₂ one therefore the sensitivity of the sensor to H₂S is significantly higher. It should also be noted that SO₂ was characterized only in the range of 20–500 ppm because of the limitation of the present gas mixing system, in which the dilution is limited to 2 % of the SO₂ gas source concentration of 2,000 ppm. However, it can be predicted from the gas sensitivity curve (Fig. 6 (b)) that the sensor does not possess appreciable sensitivity toward the exposure limit of 2–5 ppm. Thus, the sensor is not particularly suitable for SO₂ detection in atmosphere.

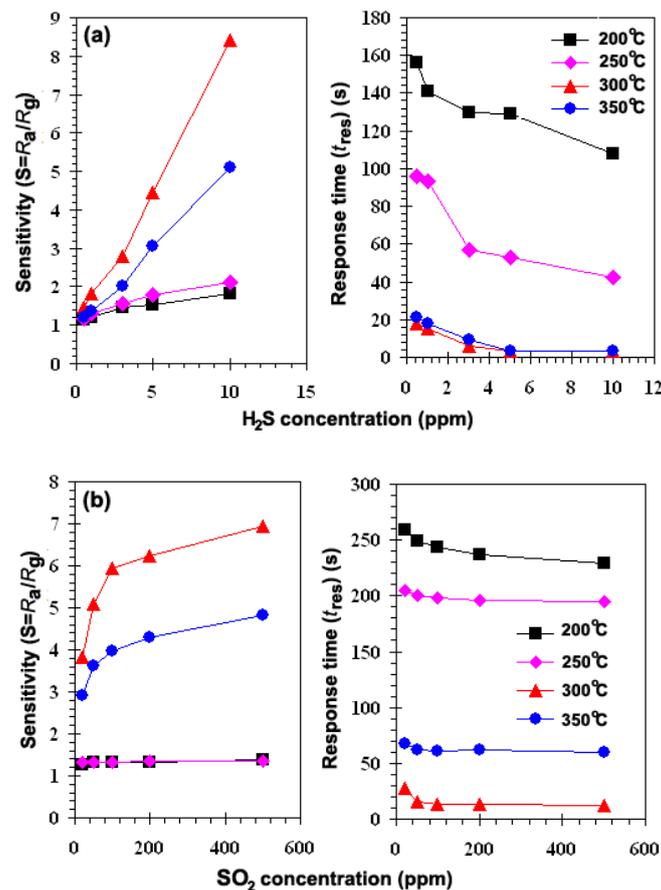


Fig. 6. Sensitivity (left) and corresponding response time (right) of SnO₂ sensors as a function of (a) H₂S and (b) SO₂ concentrations in dry air at the operating ranging from 200–350°C.

The recovery times for these gases (not shown) were within a few minutes. This is due possibly to slow desorption of gas species from highly porous SnO₂ nanostructures. This is consistent with Griessler *et al.* [5] mentioned the nanosensors based on ultrathin SnO₂ films, which were very sensitive to the highly toxic gases SO₂ and H₂S. The SnO₂-sensing films are fabricated by a spray pyrolysis process on Si substrates with a thickness of 50 nm. The sensor resistance was decreased in the presence of the toxic gases. Exposure to 50 ppm SO₂ leads to a sensor resistance drop of ~40% whereas a H₂S gas concentration of only 2.5 ppm decreases the resistance by ~85%, which demonstrates the extraordinary sensitivity of the nanosensors. Furthermore, Ghimbeu *et al.* [7] reported the ability of electrostatic sprayed SnO₂ and CuO/SnO₂ (1, 2, and 4 at.% Cu) films to detect different pollutant gases, i.e., H₂S, SO₂, and NO₂. The SnO₂ films had low response of H₂S (~6 to 10 ppm) and SO₂ (~1 to 20 ppm) at low operating temperature of 100°C. Among the studied films, the 1 at.% Cu-doped SnO₂ layer is the most sensitive in the detection of all the studied gases. Therefore, the SnO₂ sensor has been one of the most suitable candidates for the efficient detection of noxious gases for industrial environment especially H₂S at very low detection limits. The detection limit can be estimated from the characteristic curve using the standard power law for gas sensor. Taking the threshold response for detection limit of 1.05 (resistance change of 5%), the detection limits for H₂S are 0.33, 0.32, 0.35 and 0.49 ppm at 200, 250, 300 and 350°C, respectively. Similarly the detection limits for SO₂ are 5.1, 3.2, 1.0 and 1.9 ppm at 200, 250, 300 and 350°C, respectively. Thus, the sensor has optimal detection limits at 300°C operating temperature for both gases.

A summary of gas-sensing performance of pure SnO₂ prepared by various synthetic methods was shown in Table 1. It can be seen that spin-coated FSP-prepared SnO₂ film in the present work exhibits much better H₂S selectivity than other reported H₂S sensors. The sensor characteristics including response and response/recovery time of sensing films can considerably be affected by the particle morphology, size and distribution as well as operating temperature. The main advantage of FSP includes ability to produce well-controlled nanosized particles with high crystallinity structure suitable for gas sensing. However, the differences between our result and those of other flame-spray-made SnO₂ films suggest that the method for deposition of FSP nanoparticles on substrate is also very important. Spin coating technique used in this work which can produce uniform porous film with high particle density, resulting in relatively larger specific surface area and higher gas adsorption.

3.3. Environmental Selectivity

Resistive gas sensors with metal oxide layers are frequently used for monitoring environmental gases particularly toxic gases in air due to their high response and good long term stability. The cross sensitivities of the sensor towards different concentrations of H₂S, CO, H₂, and C₂H₂ were measured at 300°C (Fig. 7). The sensor evidently shows much less response to CO, H₂, and C₂H₂ than to H₂S indicating high selectivity for H₂S of the SnO₂ sensor at the lower concentration (10 ppm). The selectivity experiment for SnO₂ sensing film was carried out by monitoring changes in resistance upon exposure to several gases in both high (200 ppm, 500 ppm) and low concentration (10 ppm) ranges. The several environmental gases were also comparatively tested at the concentrations of 200 ppm for CO, and H₂S, 500 ppm for H₂ and 10 ppm for H₂S at the operating temperature of 300°C. The other environmental gases (CO, H₂, and C₂H₂) were tested at relatively high concentrations because their responses were negligible at the low concentration of 10 ppm. It can be clearly seen that the SnO₂ sensor is evidently higher selective towards H₂S through the lower concentration as it exhibits much higher resistance increase after interaction with H₂S gas molecules at the operating temperature of 300°C. On the other hand, there are much small decreases in the sensor resistance upon exposure to other interfering gases including CO, H₂ and C₂H₂.

Table 1. Summary of gas-sensing performances of pure SnO₂ materials prepared by various synthetic methods

Authors	Methods	Materials	Gas Conc.	Sensing performances		
				Response (S)	t_{res}	Selectivity
Sahm <i>et al.</i> [10]	FSP (nanopowders) Drop coating (sensors)	Pure SnO ₂	NO ₂ (10–5,000 ppb), CO (500–10,000 ppm), propanol (10–300 ppm)	NO ₂ ; ~20 to 5,000 ppb at 220°C Propanal; ~300 to 150 ppm at 220°C	-	NO ₂ ; $S \sim 20$ to 5,000 ppb
Mädler <i>et al.</i> [11]	FSP (nanopowders) Thermophoretic deposition (sensors)	0.2 wt%Pt/SnO ₂	CO; 50 ppm	8 to 50 ppm at 350°C	-	-
Jin <i>et al.</i> [3].	DC magnetron sputtering (sensors)	Pure SnO ₂ films, Ag-, Cu-, Pt-, Pd-doped SnO ₂ films (1–16 nm)	H ₂ S; 1 ppm	Doping film = 16 nm Response to H ₂ S at 200°C, 5900; 1 ppm at 250°C, 590; 1 ppm	second	-
Gong <i>et al.</i> [4]	Sol-gel	Pure SnO ₂ and Ag/SnO ₂	H ₂ S; 1–25 ppm	> 120 to 10 ppm, 70°C, 9% R.h. ~ 90 to 5 ppm, 70°C, 9% R.h. ~ 55 to 2 ppm, 70°C, 9% R.h.	-	H ₂ S, $S > 120$ to 10 ppm, 70°C Other gases; $S < 3$ Cl ₂ (10 ppm), HCl (10 ppm), HCN (10 ppm), SO ₂ (9 ppm), C ₆ H ₁₄ (0.3%), CH ₄ (2.2%), CO (50 ppm), C ₃ H ₈ (0.44%), NO ₂ (5 ppm)
Griessler <i>et al.</i> [5]	Spray pyrolysis process	Pure SnO ₂ thin film (50 ppm)	H ₂ S (2.5 ppm) and SO ₂ (50 ppm)	H ₂ S (2.5 ppm), 400°C, ~ 85% SO ₂ (50 ppm), 300°C, ~ 40%	-	-
Das <i>et al.</i> [9]	Simultaneous precipitation technique (nanopowders) Screen printing (sensor)	Pure SnO ₂ (40–50 nm) and 0.1–1 wt%V ₂ O ₅ /SnO ₂ (14–17 nm)	SO ₂ (5, 100 ppm)	Response of SO ₂ (5 ppm) at 350°C of SnO ₂ (~ 20%) and 0.15 wt%V ₂ O ₅ /SnO ₂ (~ 45%) Response to 100 ppm at 350°C of SnO ₂ (~ 35%) and 0.15 wt%V ₂ O ₅ /SnO ₂ (~ 70%)	-	$S < 30\%$ CH ₄ (100 ppm), CH ₄ H ₁₀ (100 ppm), CO (100 ppm)
Present work	FSP (nanopowders) Spin coating (sensors)	Pure SnO ₂	SO ₂ ; 20–500 ppm H ₂ S; 0.5–10 ppm	Response to 20–50 ppm of SO ₂ ~3.8–6.8, 300°C Response to 0.5–10 ppm of H ₂ S ~1.4–8.4, 300°C	500 ppm of SO ₂ 10 s, 300°C 10 ppm of H ₂ S 3 s, 300°C	Other gases like CO (200 ppm); C ₂ H ₂ (200 ppm), H ₂ (500 ppm) $S < 2$

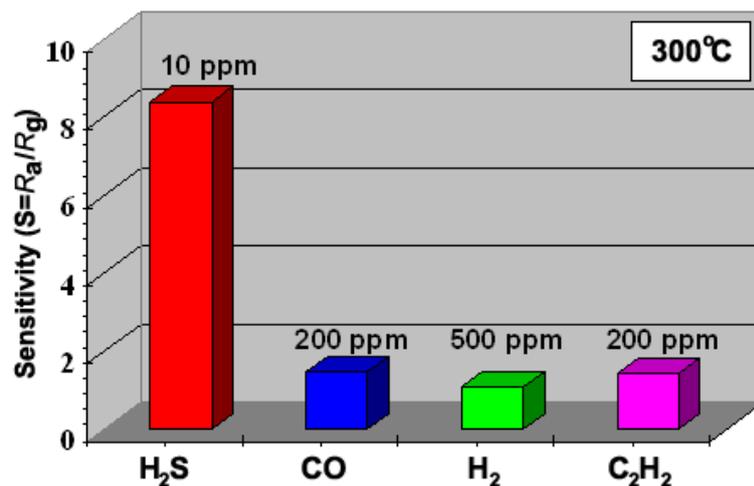


Fig. 7. The selectivity histogram of SnO₂ sensor for environmental monitoring including the H₂S, CO, H₂ and C₂H₂ at low concentration of 10 ppm for H₂S and high concentrations of 200 ppm and 500 ppm for CO, C₂H₂ and H₂, respectively, at the operating temperatures of 300°C.

3.4. Sensing Film Morphology

The cross-section, film thickness, and surface morphology of the SnO₂ sensing layer after annealing and sensing ranging from 200–350°C were observed using SEM analysis as shown in Fig. 8. It can be seen that the film thickness of sensing film is approximately 5 μm (side view), which benefits tremendously to gas-sensing properties. The SnO₂ sensing layer is crack-free and contains very high density nanoparticles. It was formed after annealing in air for binder removal at 400°C for 1h and repeated gas-sensing measurement ranging from 200–350°C. After annealing and sensing processes, a denser film layer was formed. The regularity in the film thickness stems from the uniformity of binder-powder mixing and spin coating process.

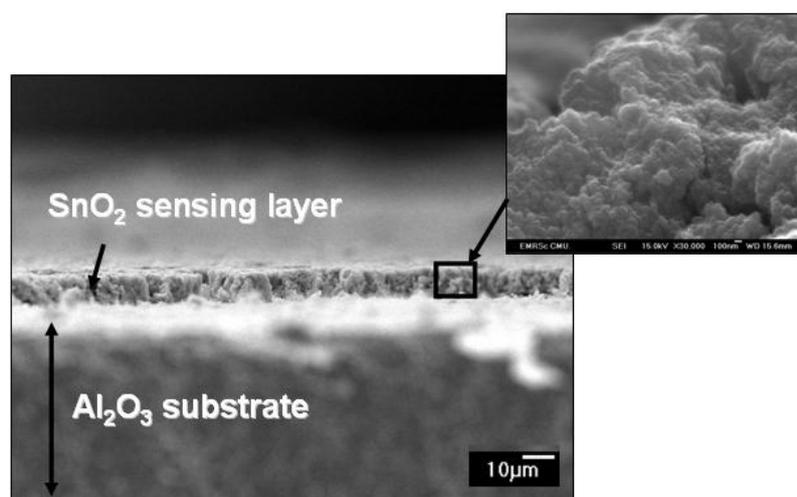


Fig. 8. SEM micrographs of SnO₂ sensing film spin-coated on an Al₂O₃ substrate with interdigitated Au electrodes after annealing at 400°C and gas-sensing measurement ranging from 200–350°C in dry air. The film thickness was approximately 5 μm.

4. Conclusions

In conclusion, the monitoring of suitable sensitive sensors for noxious gas in an industrial environment was fabricated by spin coating of flame-spray-made SnO₂ nanoparticles. The sizes and dimensional

structures (outer diameter of nanoparticles and 2D film thickness) played an important role in increasing the specific surface area of sensing layer. The nanoparticles were found to have a high specific surface area (SSA_{BET} : 141.6 m²/g), which could significantly enhance surface ionization reaction from adsorption and desorption of oxygen and gas species. The continuous sensing film was achieved leading to the connectivity of nanoparticles' properties. The SnO₂ sensor was tested to H₂S and SO₂ with different concentration ranges. The SnO₂ sensor exhibited much higher response and selectivity to H₂S (to 10 ppm, $S=8.4$) against other gases at high concentration and operating temperature of 300°C. The response time was very fast (3s) to 10 ppm of H₂S gas. Therefore, the SnO₂ sensor was one of the most suitable candidates for the efficient detection of noxious H₂S gas at low ppm-level for leakage prevention from industrial environment.

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References

- [1] C. H. Liu, L. Zhang, and Y.-J. He, "Properties and mechanism study of Ag doped SnO₂ thin films as H₂S sensors," *Thin Solid Films*, vol. 304, pp. 13–15, Feb. 1997.
- [2] R. S. Niranjana, K. R. Patil, S. R. Sainkar, and I. S. Mulla, "High H₂S-sensitive copper-doped tin oxide thin film," *Mater. Chem. Phys.*, vol. 80, pp. 250–256, Oct. 2003.
- [3] C. Jin, T. Yamazaki, K. Ito, T. Kikuta, and N. Nakatani, "H₂S sensing property of porous SnO₂ sputtered films coated with various doping films," *Vacuum*, vol. 80, pp. 723–725, 2006.
- [4] J. Gong, Q. Chen, M.-R. Lian, N.-C. Liu, R. G. Stevenson, and F. Adami, "Micromachined nanocrystalline silver doped SnO₂ H₂S sensor," *Sens. Actuators B: Chem.*, vol. 114, pp. 32–39, June 2006.
- [5] C. Griessler, E. Brunet, T. Maier, S. Steinhauer, A. Köck, T. Jordi, F. Schrank, and M. Schrems, "Tin oxide nanosensors for highly sensitive toxic gas detection and their 3D system integration," *Microelec. Eng.*, vol. 88, pp. 1779–1781, Feb., 2011.
- [6] C. M. Ghimbeu, M. Lumbreras, J. Schoonman, and M. Siadat, "Electrosprayed metal oxide semiconductor films for sensitive and selective detection of hydrogen sulfide," *Sensors*, vol. 9, pp. 9122–9132, Nov., 2009.
- [7] C. M. Ghimbeu, M. Lumbreras, M. Siadat, R. C. van Landschoot, and J. Schoonman, "Electrostatic sprayed SnO₂ and Cu-doped SnO₂ films for H₂S detection," *Sens. Actuators B: Chem.*, vol. 133, pp. 694–698, Apr. 2008.
- [8] J. Kaur, S. C. Roy, and M. C. Bhatnagar, "Highly sensitive SnO₂ thin film NO₂ gas sensor operating at low temperature," *Sens. Actuators B: Chem.*, vol. 123, pp. 1090–1095, 2007.
- [9] S. Das, S. Chakraborty, O. Parkash, D. Kumar, S. Bandyopadhyay, S. K. Samudrala, A. Sen, and H. S. Maiti, "Vanadium doped tin dioxide as a novel sulfur dioxide sensor," *Talanta*, vol. 75, pp. 385–389, Nov. 2008.
- [10] T. Sahm, L. Mädler, A. Gurlo, N. Barsan, S. E. Pratsinis, and U. Weimar, "Flame spray synthesis of tin dioxide nanoparticles for gas sensing," *Sens. Actuators B: Chem.*, vol. 98, pp. 148–153, 2004.
- [11] L. Mädler, A. Roessler, S. E. Pratsinis, T. Sahm, A. Gurlo, N. Barsan, and U. Weimar, "Direct formation of highly porous gas-sensing films by in situ thermophoretic deposition of flame-made Pt/SnO₂ nanoparticles," *Sens. Actuators B: Chem.*, vol. 114, pp. 283–295, 2005.
- [12] L. Mädler, T. Sahm, A. Gurlo, J.-D. Grunwaldt, N. Barsan, U. Weimar, and S. E. Pratsinis, "Sensing low concentrations of CO using flame-spray-made Pt/SnO₂ nanoparticles," *J. Nanopart. Res.*, vol. 8, pp. 783–796, 2006.
- [13] C. Liewhiran and S. Phanichphant, "Influence of thickness on ethanol sensing characteristics of doctor-bladed thick film from flame-made ZnO nanoparticles," *Sensors*, vol. 7, pp. 185–201, 2007.
- [14] C. Liewhiran and S. Phanichphant, "Improvement of flame-made nanoparticulate thick film morphology for ethanol sensing," *Sensors*, vol. 7, pp. 650–675, 2007.

- [15] C. Liewhiran and S. Phanichphant, "Effects of palladium loading on the response of a thick film flame-made ZnO gas sensor for detection of ethanol vapor," *Sensors*, vol. 7, pp. 1159–1184, 2007.
- [16] C. Liewhiran and S. Phanichphant "Doctor-bladed thick films of flame-made Pd/ZnO nanoparticles for ethanol sensing," *Curr. Appl. Phys.*, vol. 8, pp. 336–339, 2008.
- [17] C. Liewhiran, N. Tamaekong, A. Wisitsoraat, and S. Phanichphant, "H₂ sensing response of flame-spray-made Ru/SnO₂ thick films fabricated from spin-coated nanoparticles," *Sensors*, vol. 9, pp.8996–9010, 2009.
- [18] S. E. Pratsinis, "Flame aerosol synthesis of ceramic powders," *Prog. Energ. Combust.*, vol. 24 pp. 197–219, 1998.
- [19] L. Mädler, H. K. Kammler, R. Mueller, and S. E. Pratsinis, "Controlled synthesis of nanostructured particles by flame spray pyrolysis," *J. Aeros. Sci.*, vol. 33, pp. 369–389, 2002.
- [20] R. Mueller, L. Mädler, and S. E. Pratsinis, "Nanoparticle synthesis at high production rates by flame spray pyrolysis," *Chem. Eng. Sci.*, vol. 58, pp. 1969–1976, 2003.